



Progress on Beryllium Cavity Design R. Fernow, D. Li, R. Palmer, D. Stratakis, S. Virostek

as told to

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> NuFact10-Mumbai October 24, 2010



Introduction



- MuCool RF studies have shown significant reduction in maximum gradient when an axial magnetic field is applied
 - seen in 805 MHz test cell
 - hints of problems at 201 MHz also

 $_{\circ}$ in this case only fringe field is presently available for testing

- In both cases, it appears that problems in the coupler region are playing a strong role in observed breakdown
 - possible that further studies will change our perception of this issue
- Some models have suggested that Be may be a better wall material than Cu

motivated by this, plans to fabricate a cavity with Be walls are in progress



Present Situation



- Brief summary of experimental data shown below
 - note that behavior at 805 MHz and 201 MHz look different
 but fields are also quite different
 - "missing" 201 MHz requirement by factor of ~2





Model



- Type of data we hope to explain and mitigate:
 - damage resulting from focused field emission (a)
 - $_{\rm o}$ information from surface ohmic heating (b) provides "calibration point" on when damage can occur
 - damage believed to be caused by fatigue from repeated strains due to heating





SLAC Studies



- Used special cavity with no surface electric fields but with surface currents
 - damage observed (Tantawi *et al.*) on soft copper after cyclical heating
 $\Delta T \sim 45^{\circ}C$
 - we assume similar effect from beamlet heating







- $\boldsymbol{\cdot}$ To mitigate fatigue damage, seek materials with
 - low coefficient of thermal expansion
 - high specific heat
 - high thermal conductivity
 - for surface heating effect, also want high electrical conductivity

Materials being considered

- copper
- beryllium
 - $_{\circ}\,\text{low}\,\,\text{density}$
 - $_{\circ}$ lack of damage in experiments to date
- aluminum



Estimation of Strain



• Approach

- use approximate calculations to estimate temperature rise and resulting strain
 - $\alpha(T)$ is coefficient of thermal expansion; A_{beam} is beamlet area at surface; Q(T) is factor to account for thermal diffusion (increases transverse heat zone)
 - assumes no temperature variation with lateral diffusion

$$\Delta T \propto \frac{dE}{dx} \int_{o}^{t} \frac{Q(T)}{A_{beam} \rho C_{p}(T)} dt$$

Strain $\propto \frac{dE}{dx} \int_{o}^{t} \frac{Q(T) \alpha(T)}{A_{beam} \rho C_{p}(T)} dt$



Thermal Diffusion



- Two different assumptions made for thermal diffusion effects
 - diffusion size small compared with spot size $% \left({{{\left[{{{\left[{{{\left[{{{c}} \right]}} \right]_{{\rm{c}}}}}} \right]}_{{\rm{c}}}}} \right)$
 - $\circ \mathbf{Q}(\mathbf{T}) = \mathbf{1}$
 - diffusion size comparable to spot size
 - $_{\circ}Q(T) = d(273)/d(T)$

$$d(T) = \sqrt{\frac{K(T)\tau}{\rho C_p(T)}}$$

third option, with large diffusion size, would not match observed B dependence





Temperature Rise



- Normalized to give $\Delta T = 45^{\circ}C$ for Cu at room temperature
 - this value resulted in damage for Cu in the SLAC experiments
 - Be gives lowest temperature rise





Strain



- Use equation in slide 7 to evaluate strain for different cases
 - Be has much less strain than Cu
 - Al is somewhat better than copper
 - for case b, where thermal diffusion matters, model predicts improvement at lower temperatures for Be and Al







•Assume damage occurs at same strain as for Cu at 45°C

- Be looks better

• shape roughly consistent with what we have seen

- needs to be tested!



October 20, 2010

Accel. Concepts & Challenges - Zisman







- Beryllium appears to be ideal cavity material
 - except for fabrication issues
 - may well solve the observed gradient shortfall
- Aluminum also somewhat better than copper
 - would need TiN coating
- Be pillbox cavities would have substantial advantages over magnetically insulated cavities
 - much higher shunt impedance
 - better ratio of acceleration field to maximum surface field



Test Program (1)



- Initial tests will use back-to-back buttons
 - button field enhancement increased to 3x
 - $_{\rm o}\,$ should eliminate possibility of breakdown on Cu surfaces
 - will test Be, Al, and Cu and possibly other materials







Cavity Fabrication



- Design being done by **5**. Virostek
 - with guidance from D. Li and R. Palmer
- \cdot CAD model for one concept has been completed
 - next steps
 - ${\scriptstyle \circ}\, \text{evaluate cost of beryllium material}$
 - ${\scriptstyle \circ}$ evaluate cost of various fabrication techniques
 - ${\scriptstyle \circ}$ analyze manufacturing risks
 - brazing
 - coupling port
 - bolted joints
 - machining processes



Cavity Concept



Main features

- two bolted halves with vacuum and RF seals
 - offers accessibility advantages over e-beam welded cavity
- main body is Cu-plated Hastelloy or solid Cu
- coupling port slotted in side wall
- inner side walls are Be (TiN coated)

Side wall options

- thin Be foil (0.5 mm) brazed to side walls
- thick Be plates (6 mm) brazed to side walls
- solid Be walls (no brazing)
 - all-Be cavity probably impractical



3D CAD Model



- \cdot Initial model has been developed
 - progress delayed by other priorities recently







- Brazing
 - Be brazing is only done at select shops
 - differential expansion may be a problem for solid Cu body
 - may be some issues with brazing to Cu plated Hastelloy
 - transition from Be side walls to rounded corner at cavity OD presents some challenges
- Coupling port
 - interface between Be and cavity body material at port needs to be fully brazed
 - need to incorporate a connection flange to RF waveguide
- Cavity joints
 - seal(s) between cavity halves needs to provide a good RF connection as well as a vacuum seal
- Machining
 - few shops available to do Be machining





- Complete conceptual design layouts
- Perform analysis and trade-off studies
- Develop final conceptual design
- Generate fabrication drawings
- Procure long lead materials (Be)
- Fabricate cavity components
- Braze, coat Be and assemble cavity

LBNL responsibility (S. Virostek, D. Li)

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Summary



- Observed RF gradient in magnetic field less than required
 - SLAC sees damage due to cyclical RF heating by only 45°C
 - possible that our effect due to cyclical heating from field emitted beamlets
- Damage thresholds estimated
 - with several assumptions
- Indication that performance improved for Be cavity
 - and possibly for cavity operated at LN temperature
- Initial experiments with Be buttons planned
- \cdot Be wall cavity design under way
 - will be tested ASAP